



Investigations Supporting MOX Fuel Licensing in ESNII Prototype Reactors

Case study: SUPERFACT Integral Irradiation Experiment Fuel performance codes in fast reactors

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Framework: Do you trust scientific codes?





Oberkampf and Trucano, 2002



Framework: Validation strategy

- A Fuel Performance Code contains a lot of **different models & material properties**!
- This calls for dedicated validation strategies

STAND-ALONE VALIDATION

- Each model should be validated on its own, outside of the framework of the fuel performance code
- This is not always possible, since it requires the availability of separate effect experimental data

INTEGRAL VALIDATION

- The fuel performance code results HAVE to be compared with experimental results !
- Importance of code-to-code comparison (benchmark, w/ or w/o experimental results)
- Importance of Sensitivity Analysis and Uncertainty Analysis !!!



Framework: INSPYRE









Conducted jointly by CEA and JRC-Karlsruhe between 1984 and 1993.

Goal: demonstrate technical feasibility of transmutation of M.A. through <u>homogenous</u> (i.e., low content M.A. fuel) and heterogenous concepts (i.e., high M.A. content).

Irradiation took place in the Phénix reactor (Marcoule, France) between the 38th and 42nd cycles (October, 1986 – January, 1988), in a standard capsule containing 19 pins.

The pins selected from this database are representative of the homogenous strategy:

- SF6 and SF13 bearing 2.0 wt.% of ²³⁷Np
- SF4 and SF16 bearing 1.8 wt.% of ²⁴¹Am







The SUPERFACT irradiation experiment in a nutshell

Parameter	SF6 and SF13	SF4 and SF16		
Pellet radius (mm)	2.68	2.71		
Radial gap (mm)	0.143	0.116		
Pellet density (%TD)	97.5	96.3		
U ^a /M	0.741	0.745		
M.A. / M	0.02, ²³⁷ Np	0.018, ²⁴¹ Am		
Pu ^b /M	0.244	0.237		
0/M	1.943	1.957		
Fissile column length (mm)	850	850		
Cladding material	15-15, Ti stabilized, CW SS			
Cladding thickness (mm)	0.45	0.45		
He pressure (MPa)	0.1	0.1		



^a U nat

^{b 238}Pu 1.3%, ²³⁹Pu 60.4%, ²⁴⁰Pu 23.4%, ²⁴¹Pu 10.4%, ²⁴²Pu 4.5%





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Peak LHR vs time and Axial Peaking Factor





SUPERFACT irradiation experiment: The tools

The SUPERFACT irradiation experiment has been simulated by four of the institutions involved in the TF, with three different codes:

- **GERMINAL** (v2.2.3) CEA
- MACROS SCK CEN
- **TRANSURANUS** JRC-Karlsruhe (v1m2j17) and Polimi (v1m1j14)

The input power histories, axial peaking profile and discretization were aligned between the participants, coherently with the specifications of the irradiation experiment.

■ The codes are as-they-were **before** the project, to provide a suitable reference state for developments coming from INSPYRE.





Integral results for the Np-bearing pin

	Measured	Calculated - POLIMI (% error)	Calculated - JRC (<mark>% error</mark>)	Calculated - CEA (% error)	Calculated - SCK•CEN (% error)
Final burnup at ppn (at. %)	6.4	6.41 (<mark>0.15</mark>)	6.9 (<mark>7.8</mark>)	6.6 (<mark>3.13</mark>)	6.75 (<mark>5.47</mark>)
Fission gas (Xe + Kr) produced (cm ³)	226.68	230.96 (<mark>1.89</mark>)	231.6 (<mark>2.17</mark>)	227.24(<mark>0.25</mark>)	237.1 (<mark>4.60</mark>)
Fission gas release (%)	66.5	73.4 (<mark>10.38</mark>)	75.3(<mark>13.23</mark>)	60.6 (- <mark>8.87</mark>)	55.2 (- <mark>16.7</mark>)
Kr / (Kr + Xe) (%)	6.89	7.09 (<mark>2.9</mark>)	7.1 (<mark>3.05</mark>)	7.2 (<mark>4.50</mark>)	7.02 (<mark>1.89</mark>)
He released (cm ³)	14.2*	14.2 (<mark>0</mark>)	13.3 (<mark>-6.33</mark>)	23.8 [†] (<mark>67.6</mark>)	7.19 (- <mark>49.36</mark>)
Central hole length (mm)	624-643	850 (<mark>34</mark>)	850 (<mark>34</mark>)	598 (- <mark>5.6</mark>)	541 (- <mark>14.60</mark>)
Fuel elongation (mm)	9.5 - 10.2	23.1 (<mark>134</mark>)	24.6 (<mark>149</mark>)	3.16 (- <mark>67.9</mark>)	39.31 (<mark>299</mark>)
Clad elongation (mm)	1.6	1.42 (- <mark>11.25</mark>)	1.4 (<mark>12.5</mark>)	0.01 (- <mark>99</mark>)	1.63 (<mark>1.88</mark>)

* Measurement after 20 months from shutdown

[†] Result with a 100% release assumption





Integral results for the Am-bearing pin

	Measured	Calculated - POLIMI (<mark>% error</mark>)	Calculated - JRC (<mark>% error</mark>)	Calculated - CEA (<mark>% error</mark>)	Calculated - SCK•CEN (% error)
Final burnup at ppn (at. %)	6.4	6.23 (- <mark>2.66</mark>)	6.7 (<mark>4.68</mark>)	6.6 (<mark>3.13</mark>)	6.6 (<mark>3.13</mark>)
Fission gas (Xe + Kr) produced (cm ³)	225.03	225.98 (<mark>0.42</mark>)	226.7(<mark>0.74</mark>)	226 (<mark>0.43</mark>)	236.4 (<mark>5.05</mark>)
Fission gas release (%)	68.5	57 (<mark>-16.8</mark>)	61.5 (- <mark>10.2</mark>)	53.3 (- <mark>22.2</mark>)	53.8 (- <mark>21.4</mark>)
Kr / (Kr + Xe) (%)	6.85	6.9 (<mark>0.73</mark>)	6.9 (<mark>0.73</mark>)	7.13 (<mark>4.09</mark>)	6.94 (<mark>1.31</mark>)
He released (cm ³)	39.7*	36.3 (- <mark>8.56</mark>)	51.9(<mark>30.73</mark>)	63.9 [†] (<mark>60.9</mark>)	38 (- <mark>4.28</mark>)
Central hole length (mm)	550-619	850 (<mark>45.4</mark>)	850 (<mark>45.4</mark>)	595 (<mark>1.79</mark>)	541 (- <mark>7.44</mark>)
Fuel elongation (mm)	5.6 - 6.2	21.2 (<mark>259</mark>)	24.2 (<mark>310</mark>)	1.88 (- <mark>68</mark>)	39.13 (<mark>563</mark>)
Clad elongation (mm)	1.5 - 2.3	1.44 (- <mark>24.2</mark>)	1.4 (- <mark>26.3</mark>)	0.06 (- <mark>96.8</mark>)	1.76 (- 7.37)

* Measurement after 20 months from shutdown

[†] Result with a 100% release assumption





Comparison against local PIE: cladding profilometry



Agreement in line with SotA for all the codes, deviations likely due to different correlations for cladding steel swelling and creep, secondly to **fuel swelling** and **creep models**.





Comparison against local PIE: fuel inner diameter



Good agreement with respect to the measured values, very different trends between TRANSURANUS and MACROS&GERMINAL calculations. Many reasons could be behind those integral differences (fuel creep, gap conductance, restructuring models, relocation, cladding behavior...).







Substantial spreads in the predictions between the codes, both on predicted values and axial trends. Transuranus overprediction may be linked to a general overprediction of the temperature profile along the fuel column (with no online measurements, columnar region extent can be thought in principle to be linked to the max. local temperature).





Comparison against local PIE: Pu concentration



Local Pu concentration is linked to fuel restructuring and actinides redistribution. Satisfactory agreement for TRANSURANUS and GERMINAL predictions, MACROS does not to redistribute the actinides. Results are suggesting modeling improvements on redistribution and restructuring model parameters.



Comparison against local PIE: Xe concentration



Predictions are good in the central part (i.e., high temperatures), but suggest modeling improvements from intermediate radii, where temperatures are low and the current, simplified models employed in the codes cannot describe properly the behavior of xenon.





Code-to-code comparsion on SF13: Fuel central temperature & gap size



Different temperatures as a function of irradiation predicted by the code, especially in the first cycles. This can be partly ascribed to the different gap sizes, thus to the different gap conductance and relocation models, plus the thermal conductivity correlation employed.





Code-to-code comparsion on SF13: Fuel inner radius & cladding outer radius



Different evolution of the inner fuel void radius, due to the different restructuring model structure and parameters. Cladding evolution seems to suggest also differences in the material properties (e.g., differences in first rise to power).





Conclusions

Do you trust fuel performance codes ?





Yes, but be aware that

- They are <u>predictive tools</u>!
 - Errors cannot be cancelled by tuning...
 - They model the engineering scale of fuel pins (multi-scale...)
- Several actions HAVE to be taken to improve their confidence level
 - V & V
 - UA & SA



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Thank you for your kind attention :)

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